Alternative Earthen Final Covers: A Regulatory Perspective Bill Albright Desert Research Institute University of Nevada

for

State of California Integrated Waste Management Board and Water Resources Control Board

Introduction

- Purpose of final covers
- Regulatory review
- Liner / cover configurations
- AEFC issues: the regulatory perspective
 - Equivalency
 - How AEFCs work
 - Basic hydrology
 - Engineering philosophy
 - Defining the design process

Why Final Covers?

- Physical confinement to control spread of litter
- Control infiltration of precipitation
 - minimize production of leachate
 - minimize production of gas
- Fire control
- Limit rodent and bird contact with the refuse
- Control visual and odor aspects of facility

CALIFORNIA LAW

- Section 20950(a)(2)(A)(1), Title 27 CCR SWRCB
- "For landfills the goal of closure, including but not limited to the installation of a final cover, is to minimize the infiltration of water into the waste, thereby minimizing the production of leachate and gas."
- Section 21140(a), Title 27 CCR CIWMB
- "The final cover shall function with minimum maintenance and provide waste containment to protect public health and safety by controlling, at a minimum, vectors, fire, odor, litter and landfill gas migration. The final cover shall also be compatible with postclosure land use."
- Section 21140(c), Title 27 CCR CIWMB
- "The EA may require additional thickness, quality, and type of final cover depending on, but not limited to, the following: (1) a need to control gas emissions and fires; (2) the future reuse of the site; and (3) provide access to all areas of the site as needed for inspection of monitoring and control facilities."

ALTERNATIVES?

- Section 21090(a), Title 27 CCR SWRCB
- "The RWQCB can allow any alternative final cover design that it finds will continue to isolate the waste in the Unit from precipitation and irrigation waters as well as would a final cover built in accordance with applicable prescriptive standards."
- Section 20950(a)(2)(A)(1), Title 27 CCR SWRCB
- "For landfills the goal of closure, including but not limited to the installation of a final cover, is to minimize the infiltration of water into the waste, thereby minimizing the production of leachate and gas."
- Section 21140(b), Title 27 CCR CIWMB
- "Alternative final cover designs shall meet the requirements of part (a) [i.e., control vectors, fire, odor, litter and landfill gas migration] and shall be approved by the enforcement agency."

Prescriptive cover depends on liner design

Existing liner design	Prescriptive cover design
No liner	 30 cm erosion protection layer 30 cm barrier layer: K_{sat} ≤ 10⁻⁵ cm/sec or ≤ K_{sat} of underlying soils, whichever is less 60 cm foundation
Soil liner K _{sat} ≤ 10 ⁻⁶ cm/sec	 15 cm erosion protection layer 45 cm barrier layer with K_{sat} ≤ 10⁻⁶ cm/sec 60 cm foundation
Soil liner K _{sat} ≤ 10 ⁻⁷ cm/sec	 15 cm erosion protection layer 45 cm barrier layer with K_{sat} ≤ 10⁻⁷ cm/sec 60 cm foundation
Composite Liner: Soil layer: K _{sat} ≤ 10 ⁻⁷ cm/sec Overlain by geomembrane	 15 cm erosion protection layer Geomembrane 45 cm barrier layer with K_{sat} ≤ 10⁻⁵ cm/sec 60 cm foundation

Liner / prescriptive cover designs



Equivalency

- Equivalent hydrologic performance means percolation from AEFC ≤ percolation from prescriptive cover
- Are there data for prescriptive designs?
- Are there data for alternative designs?
- How to determine equivalency?
 - Modeling which model?
 - Side-by-side field performance

How do AEFCs work?

- Store and release
- Exploit two natural functions:
 - Water storage capacity of soil (sponge)
 - Solar powered pumps (plants)
- Can be enhanced by features such as capillary barriers

Hydrologic Components of Covers



Engineering Philosophy

- Prescriptive covers
 - Engineering by regulation
 - Can be applied anywhere
 - Based on material parameters
 - Performance not specified (not known)
- Alternative covers descriptive process
 - Site specific
 - Determine performance criterion
 - Interdisciplinary site characterization (soils, plants, climate)
 - Design and predict performance

Break

- Discussion
 - Definition of equivalency
 - Cover/liner combinations
 - Shift from prescriptive design to descriptive process: responsibilities of regulatory community

Defining the Design Process

1) Laboratory analysis of soil

Determine water storage capacity of soil (3) Hydrologic parameters (4)

Determine design precipitation event
 Seasonal for calculating water storage requirements (3)
 High resolution (daily) for numerical simulations (4)

3) Calculate required depth of soil for water storage layer

4) Numerical simulations to incorporate environmental stresses

Brief Diversion Into Hydrology and Soil Physics.....

Retention Properties - Concept



Water storage capacity of soil

- Determined from retention properties
- Retention curve (soil water characteristic curve) is determined from lab data
- Retention curve describes the relationship between water content and matric potential (soil suction, soil water potential energy, etc)
- Available water storage capacity is the difference in water content between field capacity and wilting point

Retention methods

- Hanging column
- Pressure plate apparatus
- Tempe cell apparatus
- Chilled mirror hygrometer

Hanging column



Pressure Cell Apparatus



Chilled mirror hygrometer



•Air in chamber equilibrates with soil moisture

•Mirror is cooled to dew point

•Moisture condenses on mirror, scattering light

•Dew point related to soil moisture potential

Retention Data & Fitted Curve



Available water holding capacity

•Field capacity corresponds to \sim 33 kPa

Water content

- •Wilting point corresponds to ~ 1500 kPa (6500 kPa)
- •Water holding capacity is difference in water contents between these 2 points

1 bar 100 kPa 1020 cm H₂O



Soil water potential (kPa)

Soil Textural Triangle



Important point: it is pore size distribution (not grain size distribution) that determines flow characteristics

Design Precipitation Events

- For use in calculating water storage requirements
- For use in numerical simulations
- Important regulatory decision

Precipitation Data for Calculating Water Storage Requirements

- How much water must be stored...
 - Average
 - X-yr maximum
 - Period of record
- ...and for what period of time?
 - Relative timing of precipitation (P) and transpiration (T) very important
 - During storms P > ET
 - Cold winters: T may be \sim 0 for months
 - Mild winters: P and T may coincide

Source of climate data

- Western Regional Climate Center: www.wrcc.dri.edu
- Precipitation
- PET
- Temperature

Calculation of required depth of soil for water storage layer

• Input:

Water storage capacity of soil (a) (meters of water / meter of soil)
Storage requirement (b) (meters of water)

• Calculate required depth of soil:

 $\frac{b}{-}$ = meters of soil

a

Break

- Discussion
 - Retention theory
 - Lab analysis of soil
 - Design precipitation events
 - Calculation of soil layer storage requirements

Numerical simulations (computer models)

- Purpose: to refine design by introducing environmental stress
- Regulatory concerns
 - Which model? HELP, HYDRUS-2D, UNSAT-H, LEACHM, EPIC, SoilCover, ETC-X
 - Input parameters: source?
 - Input data sets: source?
 - Results: how displayed?

Modeling: the map is not the territory

You have data?

well known, unnamed modeler

personal communication

What's a model?



.....more diversion:

Unsaturated parameters for modeling

Unsaturated soil parameters for modeling

- Models require value for unsaturated hydraulic conductivity (K_{unsat} or $K\psi$)
- Very difficult, time consuming, and expensive to <u>measure</u>
- Can be <u>estimated</u> from measured values for K_{sat} and retention properties

An aside to the diversion..... saturated vs unsaturated

- Below the water table
 - all pore space is filled with water
 - gravity dominates
- Above the water table: unsaturated (vadose) zone
 - varying degrees of air-filled porosity
 - capillary forces quickly dominate

Vadose zone hydrology (cont)

- Conceptual model is flow of water through collection of tubes – some of which may be empty
- Basic physics is Poiseuille's Law for water flow through pipes (relates flow to pipe diameter)
- Mualem combined Poiseuille's Law with various factors to describe flow of water through porous media with pores of various sizes, connected-ness, and tortuosity
- Problem: no connection to lab or field parameters
- van Genuchten described an equation that fits the shape of retention data *and* which provides the link to connect lab data to Mualem's model

Vadose zone hydrology (condensed)



 α = 1 / AEP

n = slope

Capillary barrier function



Soil Moisture Potential (kPa)

Model input: boundary conditions and internal sinks

- Represent environmental stress (boundary conditions and internal sinks) to the soil profile (modeled domain)
- Atmospheric data
- Plant community data

Atmospheric data

- Precipitation
- •Potential evapotranspiration (PET)

–Describes the ability of the atmosphere to remove water from the soil profile

- •Type of data
 - -Average
 - -10-yr
 - -Period of record
 - -Wettest 10 years on record
 - -Average all Jan. 1 data, Jan. 2 data, etc

•Requires multiple years to assure equilibrium

Plant parameters

- Ideal plant community is active year-round and roots throughout the cover
- Factors
 - Transpiration rate (internal sink)
 - Cool/warm season (time-varying boundary condition)
 - Rooting depth (location of the internal sink)
 - Sensitivity to landfill gas
 - Nutrients
- Regulatory concern: source of data

Plant community data

- •Need for modeling
 - -Location of roots in soil profile
 - –Partitioning of PET into PE and PT
 - -Seasonal timing
- •Available data
 - -Rooting depth
 - -Leaf area index
 - –Dates of freezing temperatures

Modeling and vadose zone parameters Regulatory take-home message

- Understand origin of vadose zone parameters: soil-specific parameters derived from lab measurements required for modeling
- Retention curve and K_{sat} MUST be determined by analysis of specific soil
- Describing soil *type* and then using typical vadose zone values for that *type* is not OK
- Plant data are difficult to obtain
- Design engineer / regulatory analyst interaction - agree *prior* to modeling

Pre-processing	Post-processing Graphical Display of Besults
Geometry Information Time Information Print Information Vater Flow - Iteration Criteria Vater Flow - Soil Hydraulic Model Vater Flow - Soil Hydraulic Parameters Root Water Uptake Models Root Water Uptake Models Root Water Uptake Models - Pressure Head Reduction Variable Boundary Conditions Geometry and FEM Mesh Editor Boundary Conditions Editor	 Pressure Heads Water Boundary Fluxes Cumulative Water Boundary Fluxes Soil Hydraulic Properties Run Time Information Mass Balance Information Convert Output to ASCII



Next ...



Geometry Information

Length Units

Geometry Type

🔘 <u>R</u>ectangular

🖲 <u>G</u>eneral

O mm

💽 cm.

🔘 m.



X

Time Information





Iteration Criteria



Elteration Crit	eria	
20	<u>Maximum Number of Iterations</u>	
0.0001	Water Content Tolerance	Cancel
0.1	Pressure Head <u>T</u> olerance	<u>H</u> elp
_ Time Step C	Control	
3	Lower Optimal Iteration Range	9 🙈
7	Upper Optimal Iteration Range	
1.3	Lower Time Step Multiplication Factor	<u>N</u> ext
0.7	Upper Time Step Multiplication <u>Factor</u>	<u>P</u> revious
_ Internal Inte	rpolation Tables	- Initial Condition
1e-006	Lower Limit of the Tension Interval	 In the Pressure Head
10000	Upper Limit of the Tension <u>I</u> nterval	◯ In the <u>W</u> ater Content

Soil Hydraulic Model

- Hydraulic Model
 - van <u>G</u>enuchten
 - Modified van Genuchten
 - C Brooks-Corey
- Hysteresis
- No Hysteresis
- O Hysteresis in <u>Retention Curve</u>
- \bigcirc Hysteresis in Retention Curve and <u>C</u>onductivity
 - C Initially <u>Drying</u> Curve
 - O Initially Wetting Curve

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	1	0.12	0.41	0.299	1.69	23.33	0.5			

<u>S</u> oil Catalog	•	Neural Network Prediction	□ <u>T</u> emperature Dependence		
OK Cancel	<u>H</u> elp		<u>N</u> ext	<u>P</u> revious	



Time Variable Boundary Conditions

	Time	Precip.	Evap.	Transp.	hCritA	rGWL	GWL ≜
1	5	0	0.173	0	20000	0	0-
2	6	0.7112	0.173	0	20000	0	0
3	11	0	0.173	0	20000	0	0
4	12	0.0762	0.173	0	20000	0	0
5	26	0	0.173	0	20000	0	0
6	27	0.0762	0.173	0	20000	0	0
7	32	0	0.173	0	20000	0	0
8	33	0	0.274	0	20000	0	0
9	34	0.0508	0.274	0	20000	0	0
10	55	0	0.274	0	20000	0	0
11	56	0.762	0.274	0	20000	0	0
12	60	0	0.274	0	20000	0	0 -

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I	No Flux									
	Const. Pressure									
	Const. Flux									
I	Var. Pressure									
I	Var. Flux									
I	Free Drainage									
I	Deep Drainage					••				
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ACAP

- Nationwide network of field-scale cover testing facilities
- Provides measurement (not estimate) of performance
- Side-by-side comparison of alternative with prescriptive
- Additional instrumentation to provide data for improved understanding of mechanisms and numerical estimation methods

Other monitoring methods

- Soil moisture data can be used to <u>estimate</u> performance
 - Qualitative: did a wetting front progress to depth?
 - Quantitative:Darcy's Law calculations
- These methods have problems
 - Qualitative methods rely on incorrect assumptions
 - Measurement error can lead to order-of-magnitude variation in Darcy's Law methods
- Correlating these instrument data with a single point of measurement would help

Qualitative use of instrument data to describe flux through cover (1)

- Statement: "The bottom probe(s) did not show any increase in moisture content, therefore the wetting front did not reach that depth and no flux occurred."
- Issue: If the soil at the bottom probe is at constant moisture content (and probably at unit gradient), then the soil is draining at that unsaturated hydraulic conductivity

Qualitative use of instrument data to describe flux through cover (2)

- Statement: "The bottom probe(s) did show any increase in moisture content, therefore the wetting front did reach that depth and flux did occurred."
- Issue: Even if the soil at the bottom probe shows an increase in moisture content, it may not reach the level required to drain significant water (particularly if a capillary barrier is present)

Darcy's Law calculations from soil instrument data

- A simple method to estimated flux:
 - Assume unit gradient conditions (not a bad assumption at depth)
 - Assume instrument data is very accurate
 - Flux = unsaturated hydraulic conductivity
- Issues:
 - In unsaturated conditions hydraulic conductivity is highly sensitive to moisture content
 - Small errors in measurement can translate to order-of-magnitude errors in flux estimates

Methodology and range of calculated values for instrumented (Darcy's Law calculations) estimates of cover performance



Improved monitoring methods

- ACAP-style lysimeter is probably excessive for permitting activities
- Instrumentation alone offers significant possibility of error
- Hybrid system may be considered
 - Small lysimeter
 - Some instrumentation
 - Measurement at one point can verify additional instrumented locations